

Asymmetric Variable Universe Adaptive Landing Fuzzy Controller for Carrier-Based Aircraft

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Abstract

During the process of aircraft landing, the control manners of carrier-based aircraft are always used to study. This is one of the important ways to avoid pilot-aircraft adverse coupling. In order to keep the accuracy of landing, this paper presents an improved asymmetric variable universe adaptive landing fuzzy controller with Safe Flight Area during approach for carrier-based aircraft. By means of universe-conversion factors and contraction – expansion factors, universe of discourse can be modified online, and fuzzy rules can reproduce automatically to adapt to the modified universe of discourse. The model simulation results indicate the better performance of the new method in comparison with the traditional controller with more accuracy and practicability.

Keywords: *Asymmetric Variable Universe Adaptive Fuzzy Control; Universe-Conversion Factor; Safe Flight Area; Carrier-Based Aircraft*

1. Introduction

To ensure landing on angled-deck of carrier safely and quickly during manual landing process, the pilot of carrier-based aircraft should be control flight path and attitude precisely. Landing on an aircraft carrier is usually considered by pilots as one of the most difficult exercise, complicated by visibility conditions, carrier dynamics and small landing area [1].

Considering the nonlinear, complexity and fuzziness of Landing Signal Officer, traditional control manner is not fit for “LSO-pilot-aircraft” system [2-4]. To improve control efficiency, a variable universe adaptive landing fuzzy controller should be presented. It establishes an asymmetric one as upward and downward boundaries of Safe Flight Area.

The rest of this paper is structured as follows: next section we first analyse asymmetric variable universe adaptive fuzzy controller. Section 3 designs the Safe Flight Area during approach. Multiple loading conditions simulation results show that corrective strategies is in line with the actual situation of carrier-based aircraft landing in Section 4.

2. Asymmetric Variable Universe Adaptive Fuzzy Controller

2.1. Design Universe-conversion Factors

Definition 1. Suppose XI is a standard universe, where XI with symmetric unit range $XI=[-1,1]$.

Definition 2. Since XI is a standard universe, function $\gamma: XI \rightarrow X$, $xi \rightarrow x = \gamma(xi)$ is a universe-conversion factor of the standard universe XI , if it satisfies the following axioms:

(1) Negative weighting: $\forall xi \in XI$, if $xi < 0$, then $x = \gamma(xi) = C_1(xi)$.

(2) Positive weighting: $\forall xi \in XI$, if $xi \geq 0$, then $x = \gamma(xi) = C_2(xi)$.

Where $C_j(xi) = C_j xi, (j=1,2)$ is converted function which adopted multiple weighted ways, and an ordinary universe $X = \gamma(XI) = [-C_1, C_2]$ could be obtained from a standard one with universe-conversion factor.

Definition 3. Suppose an ordinary universe $X = [-C_1, C_2]$, we call it is a symmetric universe where $C_1 = C_2$; else an asymmetric one.

If $C_1 / C_2 > 1$, X is a negative asymmetric universe;

If $C_1 / C_2 < 1$, X is a positive asymmetric universe;

If $C_1 / C_2 = 1$, X is a symmetric universe.

Definition 4. Suppose an ordinary universe $X = [-C_1, C_2]$, we call η is universe ratio item, which is indicated as:

$$\eta(x) = \begin{cases} 1, & x \geq 0 \\ C_1 / C_2, & x < 0 \end{cases} \quad (1)$$

Then

$$X = \eta(x)[-C_1, C_1] = [-\eta(x)C_1, \eta(x)C_1] = [-\eta(x)C_1, C_1] \quad (2)$$

Where C_1 is standard universe range of $X = [-C_1, C_2]$.

2.2. Design Contraction-expansion Factors

Generally speaking, a function $\alpha: X \rightarrow [0,1]$, $x \rightarrow \alpha(x)$ is called a universe contraction-expansion factor on ordinary universe $X = [-\eta C_1, C_1]$, if it satisfies the following axioms:

(1) Ratio duality: $\forall x \in X$, $\alpha(\eta(x)x) = \alpha(-\eta(x)x)$;

(2) Zero kept: $\alpha(0) = \delta$;

(3) Monotonicity: $\alpha(x)$ is strictly monotonically increasing on $[0, C_1]$, decreasing on $[-\eta C_1, 0]$;

(4) Compatibility: $\forall x \in X$, $|x| \leq \alpha(\eta(x)x)(\eta C_1)$;

(5) Normality: $\alpha(C_1) = \alpha(-\eta C_1) = 1 + \delta$.

Where δ is positive number with enough small, generally $\delta \leq \min[\eta C_1, C_1] / 1000$.

Denote sample steps to be $k = 0, 1, 2, \dots$, Contraction-expansion factor of the universe is:

$$\alpha_i(x_i^k) = \begin{cases} 1, & k = 0 \\ \left| x_i^k / \eta_i(x) C_1 \right|^\tau + \delta, & k > 0 \end{cases} \quad (3)$$

Where $\tau \in (0,1)$. If $X = [-E, E]$ is a symmetric universe, contraction-expansion factor could be denoted by

$$\alpha_i(x_i^k) = \begin{cases} 1, & k = 0 \\ |x_i^k / E|^\tau + \delta, & k > 0 \end{cases} \quad (4)$$

And the structure of a variable universe adaptive fuzzy controller is expressed in Fig.1 [5-8].

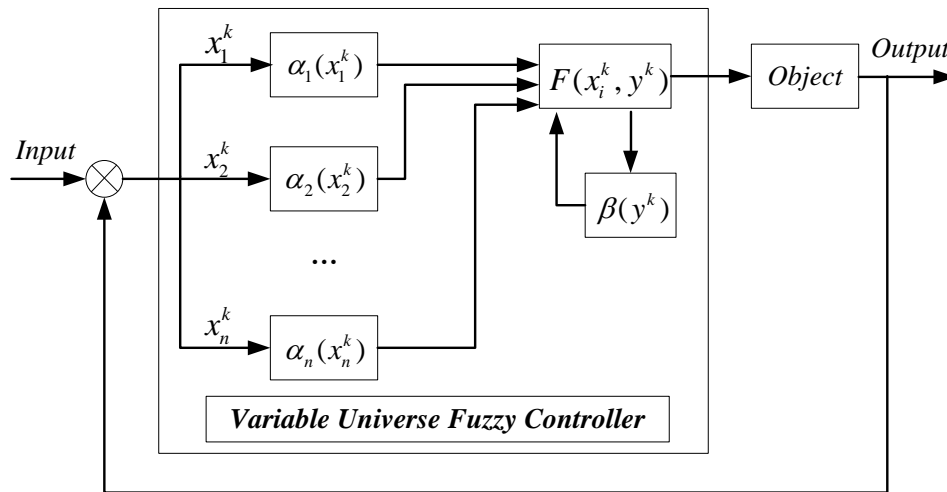


Figure 1. Variable Universe Fuzzy Controller

2.3. Design Control Algorithm of Asymmetric Variable Universe Fuzzy System

Let $U_i^0 = [-\eta C_{li}, C_{li}]$ be initial input universe of controller on the moment $k = 0$, $V^0 = [-\xi Y_l, Y_l]$ be initial output universe.

Variable universe is the universe of U_i^k and V^k varies with the change of x_i and y .

$$U_i^k = [-\eta C_{li} \alpha_i(x_i^k), C_{li} \alpha_i(x_i^k)] \quad (5)$$

$$V^k = [-\xi Y_l \beta(y^k), Y_l \beta(y^k)] \quad (6)$$

The linguistic variables are varying together with the varying of the universe, as shown in Fig2. The variable universe adaptive landing fuzzy systems can be written as shown:

$$y^{k+1} = f(\mathbf{x}^k) = \beta(y^k) \frac{\sum_{j=1}^m \bar{y}_j^0 \prod_{i=1}^n \mu_{A_{ij}^0}(\frac{x_i^k}{\alpha_i(x_i^k)})}{\sum_{j=1}^m \prod_{i=1}^n \mu_{A_{ij}^0}(\frac{x_i^k}{\alpha_i(x_i^k)})} \quad (7)$$

With the operation of $\alpha_i(x_i^k)$ and $\beta(y^k)$, the input variable universe U_i^k and the output variable universe V^k shrink or expand, and the shape of membership functions $\mu_{A_{ij}^0}$ becomes narrow or wide, as shown in Fig. 2 [9-18].

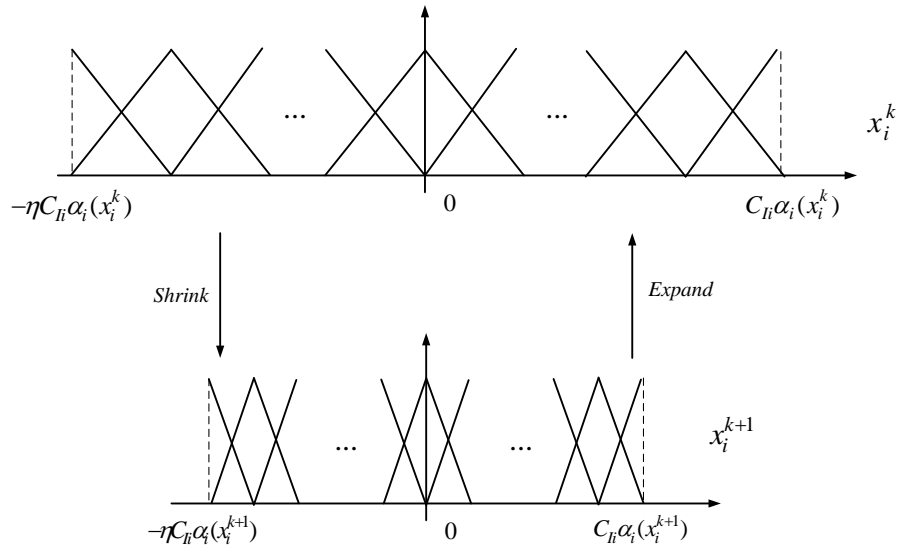


Figure 2. Shrinkage and Expansion of Universe

3. Safe Flight Area of Carrier-based Aircraft

Considering the distribution of touchdown points and hook-to-ramp clearance, Safe Flight Area envelope at different reference points will be established. In order to expound the method, IC point should be an example [3-4].

For the simulation, we consider aircraft position from the carrier is equal to 463 meters (IC point), desired velocity and angle of attack are respectively equal to 69.96 meters per second and 8.1 degrees. Preliminary glideslope deviations are varied in the range of ± 16 meters. 32 groups of the flight trajectories and touchdown points distribution are represented on Fig. 3.

As presented in Fig. 3, According to the distribution of four cables, we directly obtain the longitudinal safe rectangle area on deck of carrier: $W_{Deck} \in [-18, 30]$ m. There is a risk when touchdown point is out of the Safe Rectangle Area, so preliminary deviations should be counted by the range of touchdown points as presented in Fig. 4. The longitudinal Safe Flight Area at IC point is equal to: $z_{pIC} \in [-15.2, 11.9]$ m. To ensure the least clearance being 3 meters, the preliminary deviation at IC position is equal to: $z_{pIC} > -15.1$ m. Considering the distribution of touchdown and hook-to-ramp clearance, the longitudinal Safe Flight Area at IC point is equal to: $z_{pIC} \in [-15.1, 11.9]$ m.

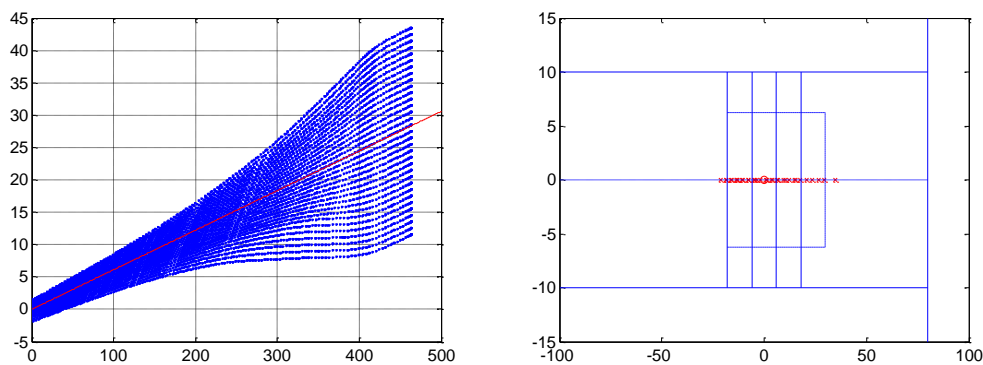


Figure 3. Flight Trajectories on IC Position and Distributions of Touchdown Points

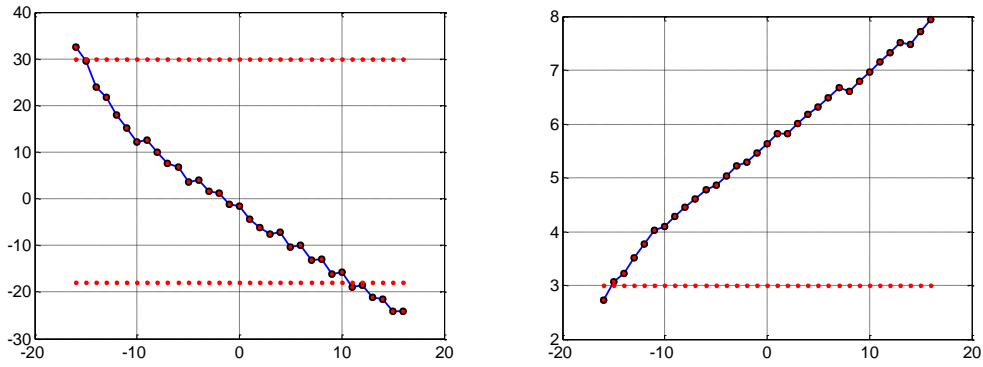


Figure 4. Relationship of Touchdown Points/ Hook-to-ramp Clearances and Deviations

Similar schemes are applied to the other reference points (X, IM, AR) as presented in Table 1.

Table 1. Safe Flight Area on Reference Positions

Reference points	Down envelope	Up envelope	Ramp Clearance	SFA boundary
X(3/4nm)	-43.5m	39.6m	>-42.8m	[-42.8,39.6]m
IM(1/2nm)	-29.2m	24.4m	>-27.7m	[-27.7,24.4]m
IC(1/4nm)	-15.2m	11.9m	>-15.1m	[-15.1,11.9]m
AR(80m)	-1.7m	2.6m	>-1.9m	[-1.7,2.6]m

4. Model Simulation

To improve the tracking precision of aircraft's trajectory, it designs Single-Input and Double-Output asymmetric variable universe adaptive fuzzy landing control system as shown in Fig.5.

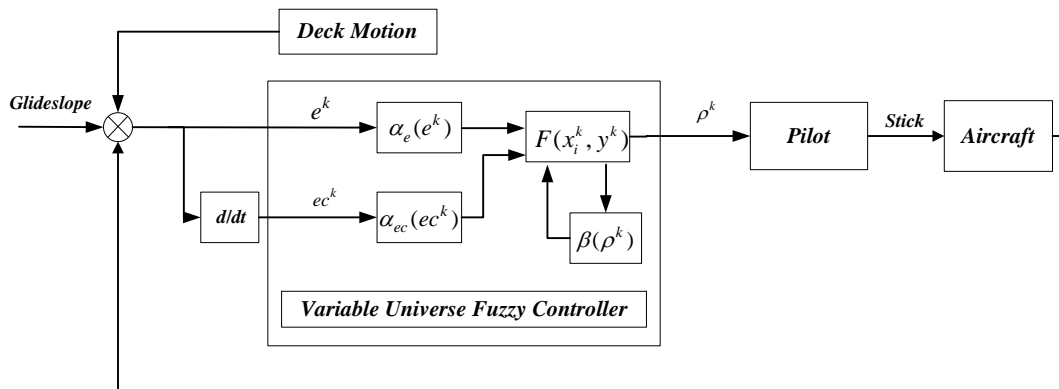


Figure 5. Variable Universe Fuzzy Trajectory Controller of Carrier-based Aircraft

The control process could be realized for some steps as follow:

Step 1. Initial universe of fuzzy control system: As safe flight area for carrier-based aircraft, $S_{FSA} = [-27.7, 24.4]m$ at reference point IM. It makes that universe ratio item $\eta = 27.7 / 24.4 = 1.135$, and the universe of e^0 is $X_e^0 = [-27.7, 24.4]$, the

universe of ec^0 is $X_{ec}^0 = [-\eta \times 5, 5] = [-5.675, 5]$, the universe of ρ^0 is $Y^0 = [-3, 3]$,

Step 2. Fuzzy division of control system: $\bar{x}_{1j}^0 (j=1, 2, \dots, 6)$ where fuzzy peak points on e^0 are divided at -27.7, -17.28, -6.86, 3.56, 13.98, 24.4; $\bar{x}_{2j}^0 (j=1, 2, \dots, 6)$ where fuzzy peak points on ec^0 are divided at -5.675, -3.54, -1.405, 0.73, 2.865, 5.

Step 3. Membership functions: Using triangle membership functions, we define $\mu_{A_j^0} (j=1, 2, \dots, 6)$ for X_e^0 as follows:

$$\mu_{A_{11}^0}(e^0) = \begin{cases} (e^0 + 17.28) / (-27.7 + 17.28) & -27.7 \leq e^0 < -17.28 \\ 0 & \text{else} \end{cases} \quad (8)$$

$$\mu_{A_{12}^0}(e^0) = \begin{cases} (e^0 + 27.7) / (27.7 - 17.28) & -27.7 \leq e^0 < -17.28 \\ (e^0 + 6.86) / (-17.28 + 6.86) & -17.28 \leq e^0 < -6.86 \\ 0 & \text{else} \end{cases} \quad (9)$$

... ..

$$\mu_{A_{16}^0}(e^0) = \begin{cases} (e^0 - 13.98) / (24.4 - 13.98) & 13.98 < e^0 \leq 24.4 \\ 0 & \text{else} \end{cases} \quad (10)$$

$\mu_{A_{2j}^0} (j=1, 2, \dots, 6)$ for X_{ec}^0 as follows:

$$\mu_{A_{21}^0}(ec^0) = \begin{cases} (ec^0 + 3.54) / (-5.675 + 3.54) & -5.675 \leq ec^0 < -3.54 \\ 0 & \text{else} \end{cases} \quad (11)$$

$$\mu_{A_{12}^0}(ec^0) = \begin{cases} (ec^0 + 5.675) / (5.675 - 3.54) & -5.675 \leq ec^0 < -3.54 \\ (ec^0 + 1.405) / (-3.54 + 1.405) & -3.54 \leq ec^0 < -1.405 \\ 0 & \text{else} \end{cases} \quad (12)$$

... ..

$$\mu_{A_{26}^0}(ec^0) = \begin{cases} (ec^0 - 2.865) / (5 - 2.865) & 2.865 < ec^0 \leq 5 \\ 0 & \text{else} \end{cases} \quad (13)$$

Step 4. Contraction-expansion factors:

$$\alpha_e(e^k) = \begin{cases} 1 & k = 0 \\ \left(|e^k| / 27.7 \right)^{0.95} + 0.01 & k = 1, 2, 3, \dots \end{cases} \quad (14)$$

$$\alpha_{ec}(ec^k) = \begin{cases} 1 & k = 0 \\ \left(|ec^k| / 5.675 \right)^{0.95} + 0.01 & k = 1, 2, 3, \dots \end{cases} \quad (15)$$

$$\beta(\rho^k) = \begin{cases} 1 & k = 0 \\ \left(\left|\rho^k\right|/3\right)^{0.95} + 0.01 & k = 1, 2, 3, \dots \end{cases} \quad (16)$$

Step 5. Fuzzy Controller is defined as follow:

$$\rho^{k+1} = \beta(\rho^k) \frac{\sum_{j=1}^{36} \bar{\rho}_j^0 \mu_{A_{1j}^0} \left(\frac{e^k}{\alpha_e(e^k)}\right) \mu_{A_{2j}^0} \left(\frac{ec^k}{\alpha_{ec}(ec^k)}\right)}{\sum_{j=1}^{36} \mu_{A_{1j}^0} \left(\frac{e^k}{\alpha_e(e^k)}\right) \mu_{A_{2j}^0} \left(\frac{ec^k}{\alpha_{ec}(ec^k)}\right)} \quad (17)$$

Fig.6-10 are the response curves of flight path, height deviation, longitudinal stick, gliding angle and velocity for different control patterns.

From Fig.6-10, the approximation error of system is $\varepsilon = 0.2$ m at the moment 3.8s under the asymmetric variable universe adaptive fuzzy landing control system, and it achieves the same error at the moment 12.3s under the traditional landing control system. It has the superiority complex on approximation error for the asymmetric variable universe adaptive fuzzy landing control system we designed.

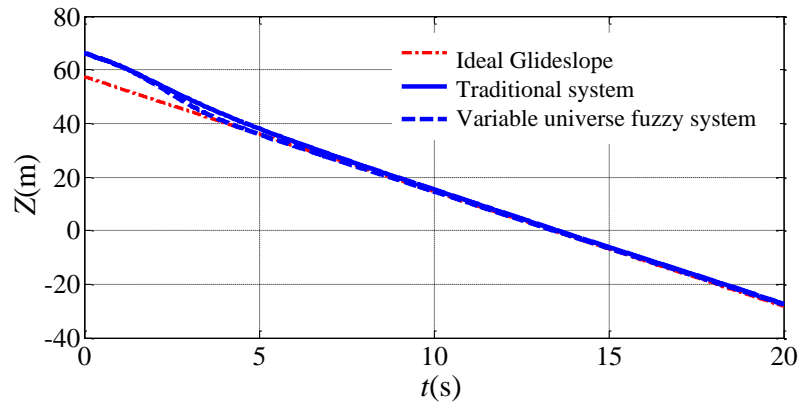


Figure 6. Response Curve of Flight Path

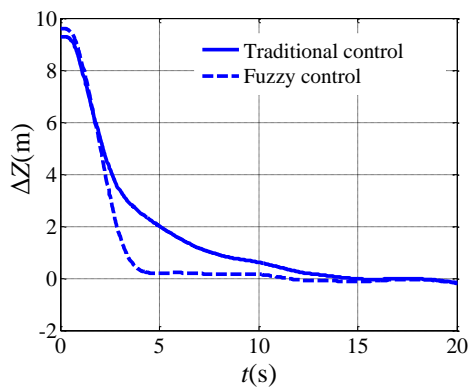


Figure 7. Response Curve of Deviation

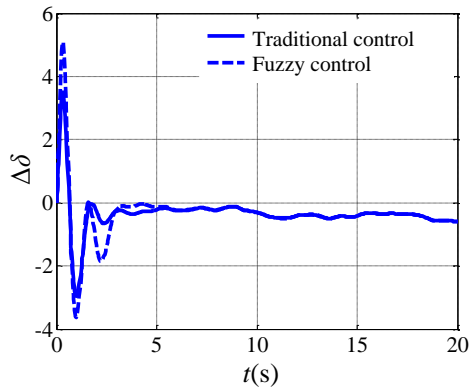


Figure 8. Response Curve of Stick

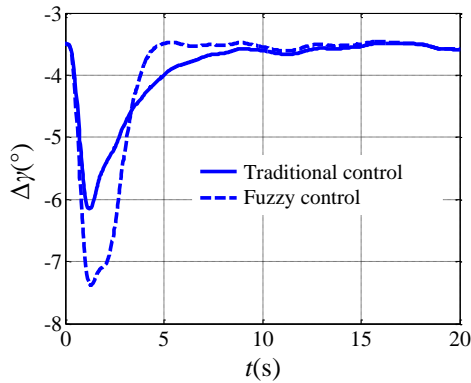


Figure 9. Response Curve of Gliding Angle

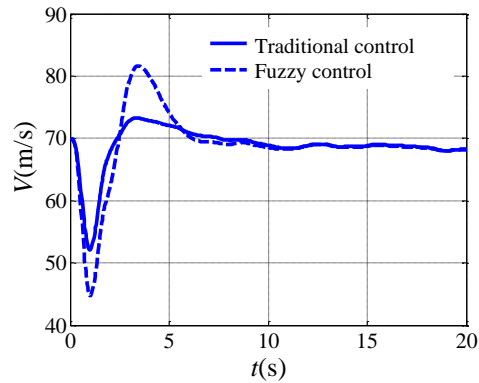


Figure 10. Response Curve of Velocity

6. Conclusion

This paper has presented an improved control manner for landing approach to perform manual landing on aircraft carrier. This asymmetric variable universe adaptive landing fuzzy controller with Safe Flight Area is established with universe-conversion factors and contraction-expansion factor. The simulation results show that compared with the traditional control manner, the fuzzy method with the SFA envelope has better evaluation result for pilots, which means more accuracy and dynamic.

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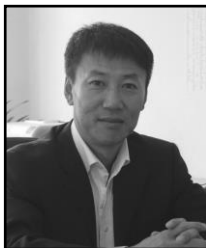
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